

# Electrified Water Disinfection and Ammonia removal via *on-site* Electrochlorination

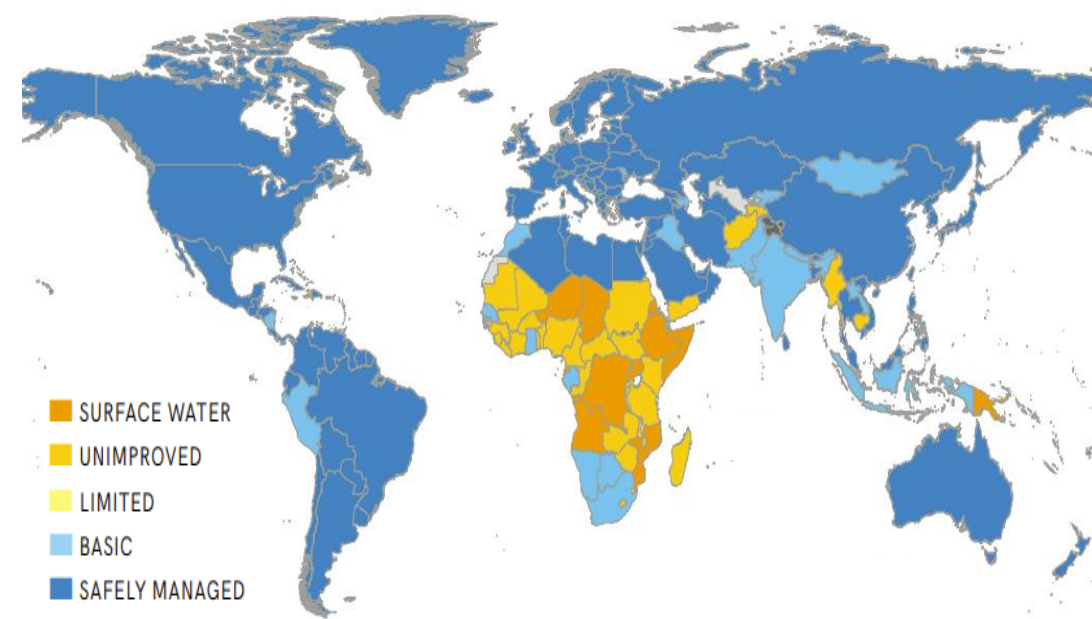
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## Introduction



29% of global population still do not have access to safely managed drinking water sources [2]

High capital cost required for centralized treatment and water distribution grids

*On-site* electrochlorination oxidizes ubiquitous chloride ions into chlorine:  $2\text{Cl}^- + 2\text{e}^- \rightarrow \text{Cl}_2$

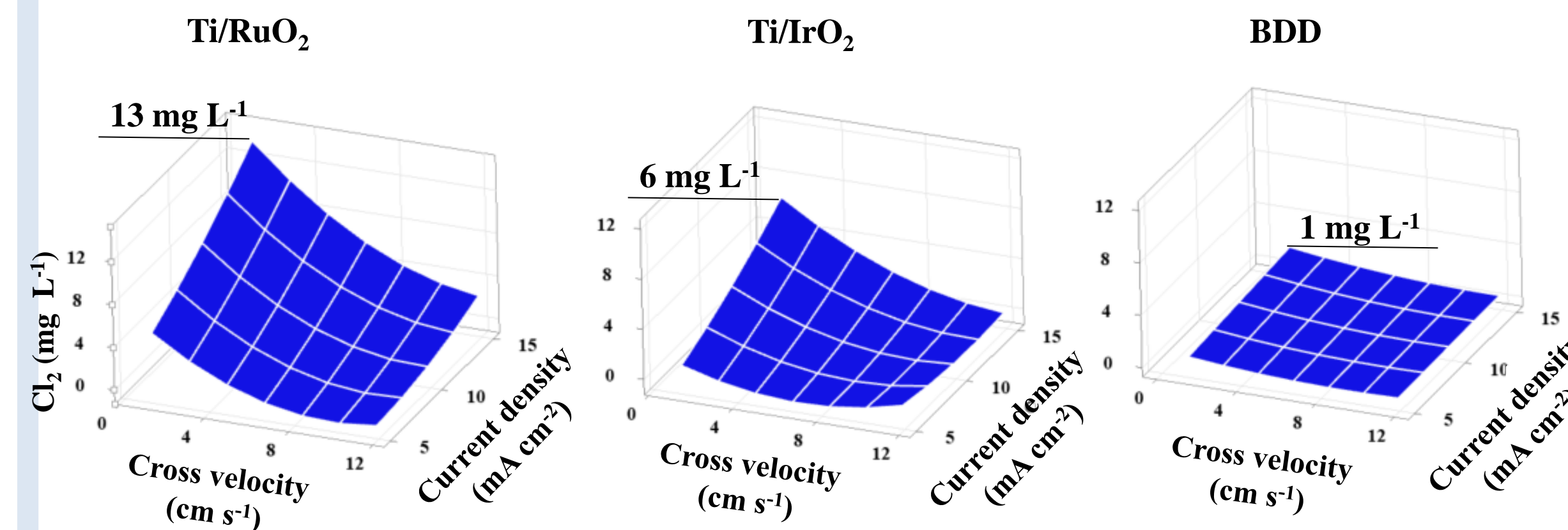
Enacts primary disinfection and provide disinfectant residuals

*On-site* electrochlorination does not require chemical addition and does not generate waste

Can be implemented for ammonia removal in ammonia contaminated waters

## Results and Discussion

### *On-site* electrochlorination for water disinfection

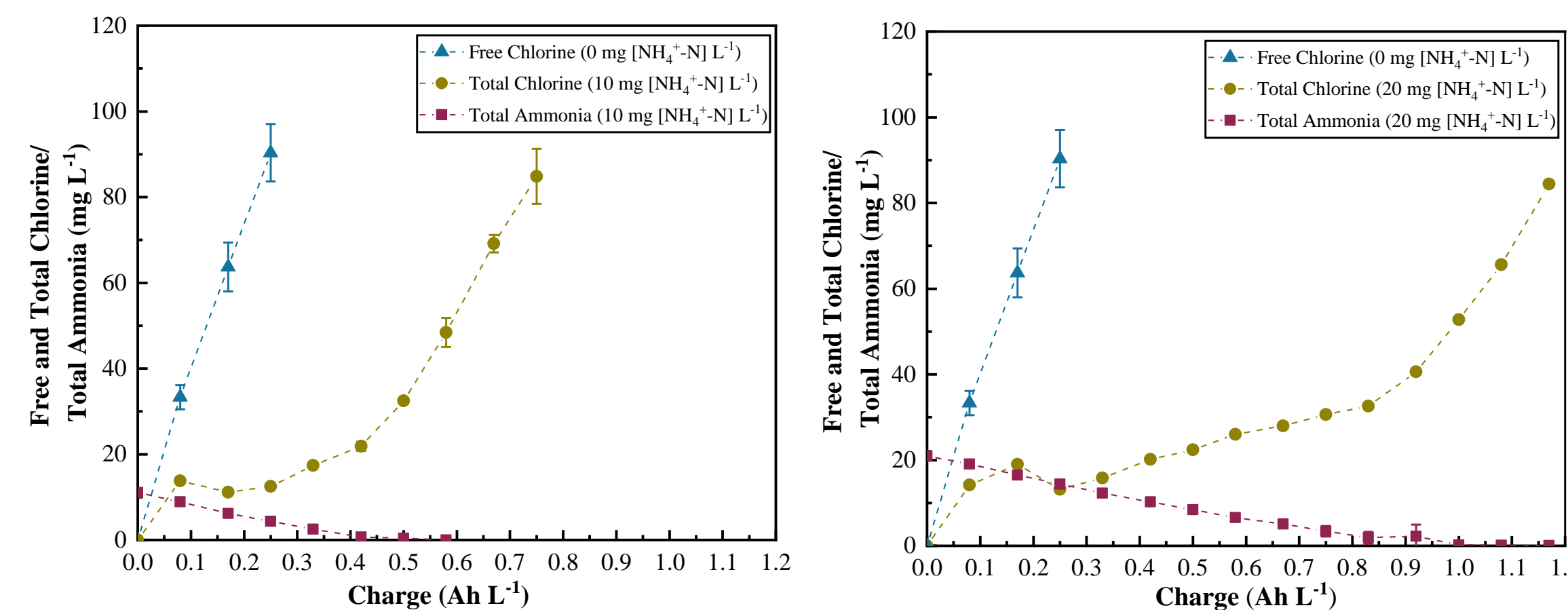


*Ti/RuO<sub>2</sub>* was evaluated as the most efficient electrocatalysts for sustained active chlorine production.

Desirable chlorine content might ne insured by selecting appropriate operating parameters.

Cross velocity was identified as the most influential parameter on active chlorine production.

### *On-site* electrochlorination for ammonia removal



Oxidation of ammonia during *on-site* electrochlorination takes place in the vicinity of the anode surface due to local excess of HOCl trough mechanism of chlorine break point.

## Conclusion

- ✓ **Ti/RuO<sub>2</sub>** was evaluated as most efficient electrocatalyst for sustained electro generation of active chlorine.
- ✓ **Desirable chlorine content might ne insured by selecting appropriate operating parameters.** Content as high as 13 ppm of active chlorine were produced in a single pass of electrochemical flow cell.
- ✓ **Cross velocity** was identified as the most influential parameter on active chlorine production.
- ✓ **Gradual total ammonia oxidation** during *on-site* electrochlorination takes place in the vicinity of the anode surface due to local excess of HOCl through mechanism of chlorine breaking point.

## Future Work

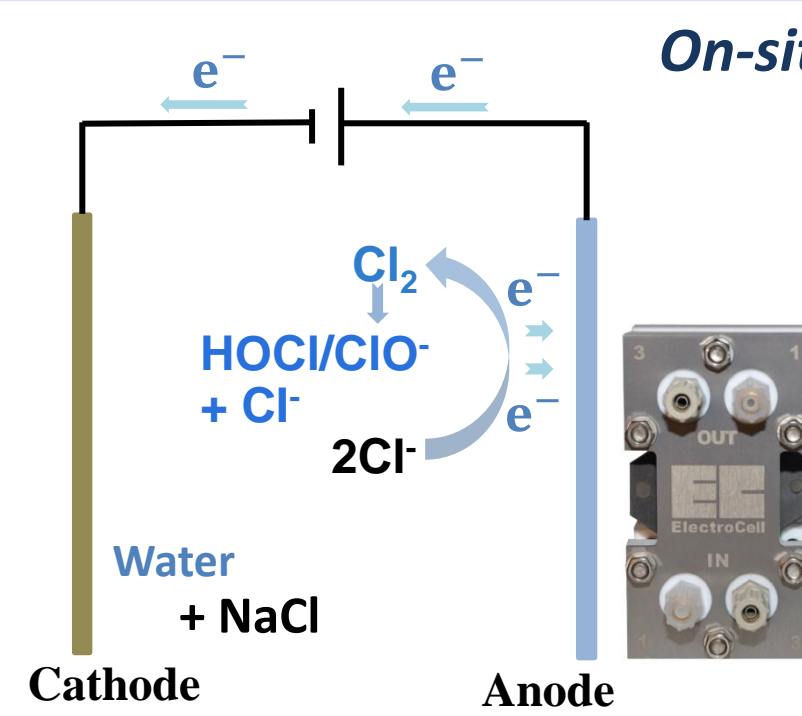
- Compare mechanism of chlorine break point during *on-site* electrochlorination with conventional chlorination.
- Evaluate mechanism of chlorine break point during *on-site* electrochlorination at different hydraulic parameters (different rotation speeds).
- Evaluate mechanism of chlorine break point during *on-site* electrochlorination at different charge transfer rates.

## References

- [1] S. Garcia-Segura, A. B. Nienhauser, A. S. Fajardo, R. Bansal, C. L. Conrad, J. D. Fortner, M. Marcos-Hernández, T. Rogers, D. Villagran, M. S. Wong and P. Westerhof, "Disparities between experimental and environmental conditions: Research steps toward making electrochemical water treatment a reality", *Current Opinion in Electrochemistry*, vol. 22, pp. 9-16, 2020.
- [2] World Health Organization, "Progress on drinking-water, sanitation and hygiene", 22 February 2018.
- [3] EPA, "Disinfection Profiling and Benchmarking. Technical Guidance and Manual", 2020.

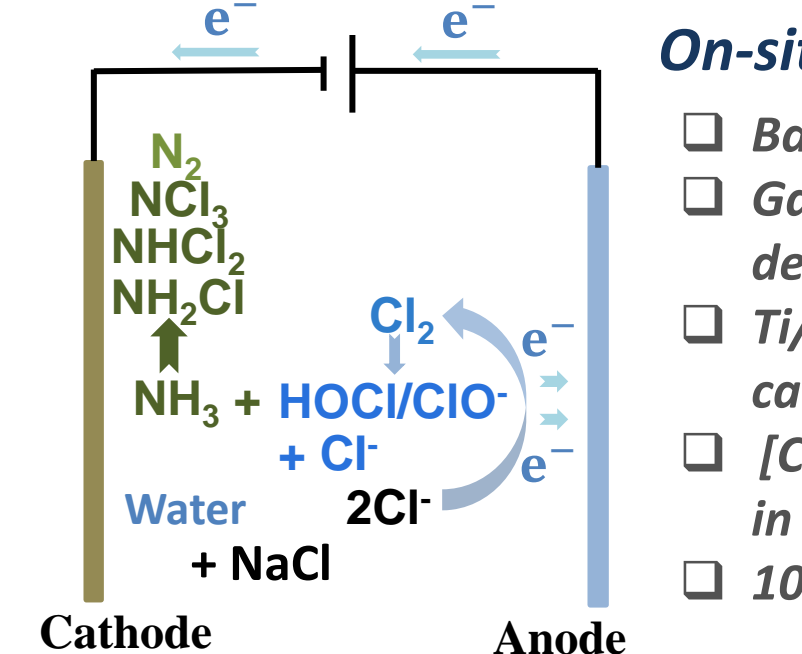
## Materials and Methods

### *On-site* electrochlorination for water disinfection



- Flow through reactor
- Cross velocities of 1.3-11.0  $\text{cm s}^{-1}$  were examined (0.1-0.9  $\text{L min}^{-1}$ )
- Galvanostatic operation mode (current densities of  $j = 5-15 \text{ mA cm}^{-2}$  were tested)
- Ti/RuO<sub>2</sub>*, *Ti/IrO<sub>2</sub>* and BDD anode materials were evaluated, and Ti plate was used as a cathode
- $[\text{Cl}^-]_0 = 50-250 \text{ mg L}^{-1}$  (below MCL of chloride for drinking water)

### *On-site* electrochlorination for ammonia removal



- Batch type reactor (0.2 L volume)
- Galvanostatic operation mode (constant current density of  $j = 17 \text{ mA cm}^{-2}$  ( $i = 0.1 \text{ A}$ ))
- Ti/IrO<sub>2</sub>* mesh as an anode and Ti plate as a cathode material
- $[\text{Cl}^-]_0 = 3000 \text{ mg L}^{-1}$  (concentration usually found in brine waters)
- 10 and 20  $\text{mg} [\text{NH}_4^+-\text{N}]_0 \text{ L}^{-1}$  were tested